

**Case Study: Taylor-Hood element**

Complete quadratic “ansatz” for each of the velocity components and linear ansatz for the pressure component in unit triangle  $S$ :

$$\begin{aligned} v(\xi, \eta) &= a_1 + a_2\xi + a_3\eta + a_4\xi^2 + a_5\xi\eta + a_6\eta^2 \\ q(\xi, \eta) &= b_1 + b_2\xi + b_3\eta \end{aligned}$$

(a) Starting from the algebraic basis

$$\Theta(\xi, \eta) = [1, \xi, \eta, \xi^2, \xi\eta, \eta^2]T$$

the basis  $\Psi = [\psi_1, \dots, \psi_6]$  of shape functions in unit triangle is calculated by means of the design matrix  $B$ :

$$\Psi(\xi, \eta) = \Theta(\xi, \eta)B. \quad (1)$$

in succession  $(0, 0), (1, 0), (0, 1), (1/2, 0), (1/2, 1/2), (0, 1/2)$

$$\begin{aligned} u_1 = v(0, 0) &= a_1 \\ u_1 = v(1, 0) &= a_1 + a_2 + a_4 \\ u_3 = v(0, 1) &= a_1 + a_3 + a_5 \\ u_4 = v(1/2, 0) &= a_1 + a_2/2 + a_4/4 \\ u_5 = v(1/2, 1/2) &= a_1 + a_2/2 + a_3/2 + a_4/4 + a_5/4 + a_6/4 \\ u_6 = v(0, 1/2) &= a_1 + a_3/2 + a_6/4 \end{aligned}$$

It follows  $\underline{u} = A\underline{a}$ ,  $\underline{a} = B\underline{u}$  where

$$A = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 0 & 1 & 0 & 0 \\ 1 & 0 & 1 & 0 & 0 & 1 \\ 1 & 1/2 & 0 & 1/4 & 0 & 0 \\ 1 & 1/2 & 1/2 & 1/4 & 1/4 & 1/4 \\ 1 & 0 & 1/2 & 0 & 0 & 1/4 \end{bmatrix}, \quad B = A^{-1} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ -3 & -1 & 0 & 4 & 0 & 0 \\ -3 & 0 & -1 & 0 & 0 & 4 \\ 2 & 2 & 0 & -4 & 0 & 0 \\ 4 & 0 & 0 & -4 & 4 & -4 \\ 2 & 0 & 2 & 0 & 0 & -4 \end{bmatrix}.$$

and then, by (1),

$$\begin{aligned} \psi_1 &= (1 - \xi - \eta)(1 - 2\xi - 2\eta) = \zeta_1(2\zeta_1 - 1) \\ \psi_2 &= \xi(2\xi - 1) = \zeta_2(2\zeta_2 - 1) \\ \psi_3 &= \eta(2\eta - 1) = \zeta_3(2\zeta_3 - 1) \\ \psi_4 &= 4\xi(1 - \xi - \eta) = 4\zeta_1\zeta_2 \\ \psi_5 &= 4\xi\eta = 4\zeta_2\zeta_3 \\ \psi_6 &= 4\eta(1 - \xi - \eta) = 4\zeta_1\zeta_3 \end{aligned}$$

Now we calculate the following matrices in unit triangle

$$\begin{aligned} S_1 &= \int_S \Psi_\xi \Psi_\xi^T d\xi d\eta, & S_2 &= \int_S [\Psi_\xi \Psi_\eta^T + \Psi_\eta \Psi_\xi^T] d\xi d\eta \\ S_3 &= \int_S \Psi_\eta \Psi_\eta^T d\xi d\eta, & S_4 &= \int_S \Psi \Psi^T d\xi d\eta \end{aligned}$$

then

$$S_1 = \frac{1}{6} \begin{bmatrix} 3 & 1 & 0 & -4 & 0 & 0 \\ 1 & 3 & 0 & -4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -4 & -4 & 0 & 8 & 0 & 0 \\ 0 & 0 & 0 & 0 & 8 & -8 \\ 0 & 0 & 0 & 0 & -8 & 8 \end{bmatrix}, \quad S_2 = \frac{1}{6} \begin{bmatrix} 6 & 1 & 1 & -4 & 0 & -4 \\ 1 & 0 & -1 & -4 & 4 & 0 \\ 1 & -1 & 0 & 0 & 4 & -4 \\ -4 & -4 & 0 & 8 & -8 & 8 \\ 0 & 4 & 4 & -8 & 8 & -8 \\ -4 & 0 & -4 & 8 & -8 & 8 \end{bmatrix},$$

$$S_3 = \frac{1}{6} \begin{bmatrix} 3 & 0 & 1 & 0 & 0 & -4 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 3 & 0 & 0 & -4 \\ 0 & 0 & 0 & 8 & -8 & 0 \\ 0 & 0 & 0 & -8 & 8 & 0 \\ -4 & 0 & -4 & 0 & 0 & 8 \end{bmatrix}, \quad S_4 = \frac{1}{360} \begin{bmatrix} 6 & -1 & -1 & 0 & -4 & 0 \\ -1 & 6 & -1 & 0 & 0 & -4 \\ -1 & -1 & 6 & -4 & 0 & 0 \\ 0 & 0 & -4 & 32 & 16 & 16 \\ -4 & 0 & 0 & 16 & 32 & 16 \\ 0 & -4 & 0 & 16 & 16 & 32 \end{bmatrix},$$

Likewise one calculates the shape functions for linear approximation in unit triangle:

$$\tilde{\Psi} = [1 - \xi - \eta, \xi, \eta]^T$$

and the both integrals

$$C_1 = \int_S \Psi_\xi \tilde{\Psi}^T d\xi d\eta = \frac{1}{6} \begin{bmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \\ 1 & -1 & 0 \\ 1 & 1 & 2 \\ -1 & -1 & -2 \end{bmatrix}, \quad C_2 = \int_S \Psi_\eta \tilde{\Psi}^T d\xi d\eta = \frac{1}{6} \begin{bmatrix} -1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -1 \\ 1 & 2 & 1 \\ 1 & 0 & -1 \end{bmatrix}$$

and

$$S_5 = \int_S \Psi \tilde{\Psi}^T d\xi d\eta = \frac{1}{24} \begin{bmatrix} 2 & 1 & 1 \\ 1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix}.$$

Stationary NAVIER-STOKES equations with convection term:

$$\begin{aligned} a(\underline{v}, \underline{u}) + c(\underline{v}, \underline{u}, \underline{u}) - (\operatorname{div} \underline{v}, p) &= (\underline{v}, \underline{f}) + (\underline{v}, \underline{\sigma}_n(\underline{u}, p))_\Gamma, \quad \underline{v} \in \mathcal{V} \\ -(\operatorname{div} \underline{v}, q) &= 0, \quad q \in \mathcal{Q} \\ \underline{\sigma}_n(\underline{u}, p) &= (2\nu \underline{\varepsilon}(\underline{u}) - p) \underline{n} \end{aligned}$$

In arbitrary triangle  $T(x, y)$  we have

$$\begin{aligned} a(\underline{u}, \underline{v}) &= \nu \int_T \operatorname{grad} \underline{u} : \operatorname{grad} \underline{v} \, dx dy \\ &= \nu \int_T [u_{1,x} v_{1,x} + u_{1,y} v_{1,y}] \, dx dy + \nu \int_T [u_{2,x} v_{2,x} + u_{2,y} v_{2,y}] \, dx dy \\ &= \tilde{a}(u_1, v_1) + \tilde{a}(u_2, v_2) \\ b(\underline{u}, q) &= \int_T \operatorname{div} \underline{u} \cdot q \, dx dy = \int_T (u_{1,x} + u_{2,y}) q \, dx dy \\ c(\underline{u}, \underline{v}, \underline{w}) &= \int_T \underline{u} \cdot (\operatorname{grad} \underline{v}) \underline{w} \, dx dy \end{aligned}$$

For transformation on the unit triangle we have e.g.

$$\begin{aligned}
b(\underline{u}, q) &= \int_T (u_{1,\xi}\xi_x + u_{1,\eta}\eta_x) q \, dx dy + \int_T (u_{2,\xi}\xi_y + u_{2,\eta}\eta_y) q \, dx dy \\
&= J \int_S (u_{1,\xi}\xi_x + u_{1,\eta}\eta_x) q \, d\xi d\eta + J \int_S (u_{2,\xi}\xi_y + u_{2,\eta}\eta_y) q \, d\xi d\eta \\
&= \frac{J}{J} U_1^T (C_1 y_{31} - C_2 y_{21}) Q + \frac{J}{J} U_2^T (C_2 x_{21} - C_1 x_{31}) Q,
\end{aligned}$$

where  $U_1, U_2 \in \mathbb{R}^6$ ,  $Q \in \mathbb{R}^3$  are the local vectors of the node variables in the triangle

**(b) Trilinear Form** with shape functions.

$$P(\underline{u}, \underline{v}, \underline{w}) = \underline{u}^T [\text{grad } \underline{v}] \underline{w}$$

$$\underline{u} \simeq \begin{bmatrix} \Phi(x, y)^T U_1 \\ \Phi(x, y)^T U_2 \end{bmatrix},$$

$$N(\underline{u}, \underline{v}, \underline{w}) \simeq [U_1^T, U_2^T] \begin{bmatrix} (\Phi_x^T V_1) \Phi \Phi^T & (\Phi_y^T V_1) \Phi \Phi^T \\ (\Phi_x^T V_2) \Phi \Phi^T & (\Phi_y^T V_2) \Phi \Phi^T \end{bmatrix} \begin{bmatrix} W_1 \\ W_2 \end{bmatrix},$$

$$\Phi_x = \Psi_\xi \xi_x + \Psi_\eta \eta_x, \quad \Phi_y = \Psi_\xi \xi_y + \Psi_\eta \eta_y,$$

$$\int_T N(\underline{u}, \underline{v}, \underline{w}) \simeq [U_1^T, U_2^T] \begin{bmatrix} A(V_1) & B(V_1) \\ C(V_2) & D(V_2) \end{bmatrix} \begin{bmatrix} W_1 \\ W_2 \end{bmatrix},$$

where

$$\begin{aligned}
A(V_1) &= J \int_S ((\Psi_\xi \xi_x + \Psi_\eta \eta_x)^T V_1) \Psi \Psi^T \, d\xi d\eta, \\
B(V_1) &= J \int_S ((\Psi_\xi \xi_y + \Psi_\eta \eta_y)^T V_1) \Psi \Psi^T \, d\xi d\eta \\
C(V_2) &= J \int_S ((\Psi_\xi \xi_x + \Psi_\eta \eta_x) V_2) \Psi \Psi^T \, d\xi d\eta, \\
D(V_2) &= J \int_S ((\Psi_\xi \xi_y + \Psi_\eta \eta_y) V_2) \Psi \Psi^T \, d\xi d\eta
\end{aligned} \tag{2}$$

Now we have the representation

$$\begin{aligned}
\Psi_\xi &= \begin{bmatrix} -3 & 4 & 4 \\ -1 & 4 & 0 \\ 0 & 0 & 0 \\ 4 & -8 & -4 \\ 0 & 0 & 4 \\ 0 & 0 & -4 \end{bmatrix} \begin{bmatrix} 1 \\ \xi \\ \eta \end{bmatrix} =: [A_1, A_2, A_3] \begin{bmatrix} 1 \\ \xi \\ \eta \end{bmatrix} \\
\Psi_\eta &= \begin{bmatrix} -3 & 4 & 4 \\ 0 & 0 & 0 \\ -1 & 0 & 4 \\ 0 & -4 & 0 \\ 0 & 4 & 0 \\ 4 & -4 & -8 \end{bmatrix} \begin{bmatrix} 1 \\ \xi \\ \eta \end{bmatrix} =: [B_1, B_2, B_3] \begin{bmatrix} 1 \\ \xi \\ \eta \end{bmatrix}
\end{aligned}$$

Accordingly, only the both matrices  $P, Q$  are to be calculated:

$$M := S_4 = \int_S \Psi \Psi^T \, d\xi d\eta, \quad P = \int_S \xi \Psi \Psi^T \, d\xi d\eta, \quad Q = \int_S \eta \Psi \Psi^T \, d\xi d\eta,$$

Then we obtain

$$\begin{aligned}\int_S (\Psi_\xi V) \Psi \Psi^T d\xi d\eta &= (A_1^T V)M + (A_2^T V)P + (A_3^T V)Q \\ \int_S (\Psi_\eta V) \Psi \Psi^T d\xi d\eta &= (B_1^T V)M + (B_2^T V)P + (B_3^T V)Q\end{aligned}$$

and the integrals (2) are linear combinations of these both integrals with the corresponding arguments  $V_1$  resp.  $V_2$

$$\begin{aligned}A(V_1) &= [(A_1 y_{31} - B_1 y_{21})V_1]M + [(A_2 y_{31} - B_2 y_{21})V_1]P + [A_3 y_{31} - B_3 y_{21}]V_1]Q \\ B(V_1) &= [(-A_1 x_{31} + B_1 x_{21})V_1]M + [(-A_2 x_{31} + B_2 x_{21})V_1]P + [(-A_3 x_{31} + B_3 x_{21})V_1]Q \\ C(V_2) &= [(A_1 y_{31} - B_1 y_{21})V_2]M + [(A_2 y_{31} - B_2 y_{21})V_2]P + [A_3 y_{31} - B_3 y_{21}]V_2]Q \\ D(V_2) &= [(-A_1 x_{31} + B_1 x_{21})V_2]M + [(-A_2 x_{31} + B_2 x_{21})V_2]P + [(-A_3 x_{31} + B_3 x_{21})V_2]Q\end{aligned}$$

(c) The nonlinear problem may be solved by a simple iteration method or by NEWTON's method. The latter allows higher REYNOLDS numbers  $Re = 1/\nu$ . Also, in NEWTON's method the gradient of the nonlinear part must be calculated. From (b)

$$\text{grad}_{U_1, U_2} \begin{bmatrix} A(U_1) & B(U_1) \\ C(U_2) & D(U_2) \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \end{bmatrix} = \begin{bmatrix} A(U_1) & B(U_1) \\ C(U_2) & D(U_2) \end{bmatrix} + \begin{bmatrix} A(U_1) & \text{Null} \\ \text{Null} & D(U_2) \end{bmatrix}$$

(d) **Postprozessor** Let  $\underline{u} = (u, v)$  be the velocity field then the streamlines  $z$  satisfy

$$\begin{aligned}\int_\Omega \nabla \delta z \nabla z &= \int_\Omega \delta z w + \int_\Gamma \delta z z_{\underline{n}} \\ \int_T \varphi_i w &= \int_T \varphi_i (v_x - u_y) + \int_\Gamma \delta z z_{\underline{n}} \\ \int_T \delta z w dx dy & \\ &\simeq JZ \int_S \Psi (\Psi_\xi \xi_x + \Psi_\eta \eta_x)^T d\xi d\eta V - JZ \int_S \Psi (\Psi_\xi \xi_y + \Psi_\eta \eta_y)^T d\xi d\eta U \\ &= JZ \left[ \int_S \Psi \Psi_\xi^T d\xi d\eta \right] (V \xi_x - U \xi_y) + JZ \left[ \int_S \Psi \Psi_\eta^T d\xi d\eta \right] (V \eta_x - U \eta_y)\end{aligned}$$

Accorcingly, the matrices

$$\int_S \Psi \Psi_\xi^T d\xi d\eta, \quad \int_S \Psi \Psi_\eta^T d\xi d\eta$$

are to be calculated.